

# Crystallization and melting behaviors of maleic anhydride grafted poly(propylene) nucleated by an aryl amide derivative

Bo Song · Yong Wang · Hongwei Bai · Li Liu · Yanli Li · Jihong Zhang · Zuowan Zhou

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**Abstract** This paper reports the crystallization behavior of maleic anhydride grafted poly(propylene) (PP-MA) with an aryl amide derivative (TMB-5) as  $\beta$ -phase nucleating agent ( $\beta$ -NA). The isothermal and nonisothermal crystallization behaviors of PP-MA and nucleated PP-MA are comparatively researched based on the concentration of  $\beta$ -NA of 0.2 wt%. Subsequent melting behaviors after isothermal and nonisothermal crystallization process are also investigated to explore the crystalline structures formed during the crystallization. The results indicate that TMB-5 is an efficient  $\beta$ -NA in influencing the crystallization of PP-MA through increasing the crystallization rate and decreasing the fold surface free energy, leading to large amounts of  $\beta$ -phase formation during the crystallization process.

**Keywords** Aryl amide derivative · Isothermal and nonisothermal crystallization · Melting · PP-MA

## Introduction

Isotactic poly(propylene) (iPP) is well known for its three common crystal forms,  $\alpha$ ,  $\beta$  and  $\gamma$  modification [1]. Among these crystal forms,  $\beta$ -PP has received considerable

interests due to its excellent thermal and mechanical performance, especially high impact strength at low temperature [2, 3]. However,  $\beta$ -PP is in a metastable phase, it can be rarely obtained in a significant amount in commercial iPP products, unless crystallization conditions facilitating to the  $\beta$ -phase growth are taken [4, 5], such as quenching the melt to a certain temperature range [6], directional crystallization in a thermal gradient field [4, 5], shearing or elongation of the melt during crystallization process [7–10], vibration-induced crystallization [11], or using  $\beta$ -nucleating agent ( $\beta$ -NA) [2]. Of these methods, the addition of  $\beta$ -NA is the most effective to obtain a high level of the  $\beta$ -phase. The role of  $\beta$ -NA in inducing PP crystallization has been intensively researched. It has been widely accepted by researchers that the crystallization of PP nucleated by a NA includes two steps: one is the epitaxial growth of PP chain on the surface of the NA and the other is the growth of PP spherulites [12]. A certain epitaxial relationship between PP and the nucleating agent controls and accelerates heterogeneous nucleation and, finally determines the nucleation efficiency of such NA.

In the present work, maleic anhydride grafted poly(propylene) (PP-MA) was used and it is of considerable industrial interest to enhance its compatibility, adhesion and reactivity [13]. Aryl amides derivative (TMB-5) was used as  $\beta$ -NA for PP-MA. In the previous work, TMB-5 has been proved to be an efficient NA for iPP [14]. Here, we attempted to research the nucleation effect of TMB-5 on crystallization of PP-MA. The  $\beta$ -crystallization tendency of PP-MA has been reported recently [15]. Isothermal and nonisothermal crystallization behaviors and subsequent melting behaviors of nucleated PP-MA and neat PP-MA were comparatively researched through differential scanning calorimetry (DSC), polarized light microscope (PLM) and wide angle X-ray diffraction (WAXD) in this work.

B. Song · Y. Wang (✉) · H. Bai · L. Liu · Y. Li · J. Zhang · Z. Zhou  
Key Laboratory of Advanced Technologies of Materials  
(Ministry of Education), School of Materials Science & Engineering, Southwest Jiaotong University, Chengdu 610031, China  
e-mail: yongwang1976@163.com

## Experimental

### Materials

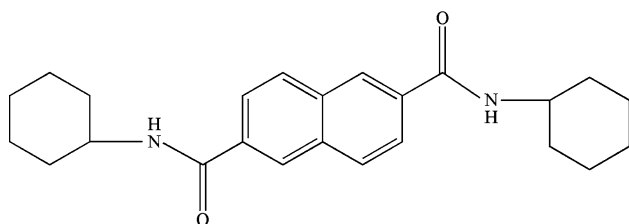
PP-MA (melt flow rate (MFR) of 29 g/10 min, 230 °C/2.16 kg) was obtained from Chengguang Institute of Chemical Engineering, China. MA group was randomly grafted onto the PP backbone, and the MA content in PP is 0.6 wt%. The  $\beta$ -phase NA aryl amides derivative (trade-mark: TMB-5) was supplied by Fine Chemicals Department of Shanxi Provincial Institute of Chemical Industry, China. Although we can not know the detailed chemical structure of this NA, it has been reported that TMB-5 has the similar chemical structure compared with some aromatic amine  $\beta$ -phase NA, such as *N,N'*-dicyclohexyl-2,6-naphthalenedicarboxamide, as shown in Scheme 1.

### Sample preparation

Both PP-MA and NA were dried in an oven at 80 °C for 2 h prior to melt blending to eliminate the effect of moisture. A certain composition of PP-MA with 0.2 wt% NA (Shown as PP-MA/NA) was melt blended through using a Lab-station Brabender torque rheometer (Plasti-Corder, Germany) with the setting temperature of 185 °C. The melt blending time was 10 min and the rotor speed was 60 rpm. To provide same thermal history for both PP-MA and its nucleated sample, neat PP-MA was treated using exactly the same procedure as above. After that, the melt was cooled in the air.

### Characterization

A Pyris-1 of Perkin-Elmer DSC was used for calorimetric investigation of the isothermal/non-isothermal crystallization and subsequent melting behaviors of samples. For isothermal crystallization process, about 5.0 mg sample was heated to 200 °C to erase the thermal history. After that, the sample was cooled down to a predetermined crystallization temperature at a cooling rate of 100 °C/min and crystallized at this temperature until the crystallization was finished



**Scheme 1** Chemical structure of *N,N'*-dicyclohexyl-2,6-naphthalenedicarboxamide

completely. Subsequently, the sample was heated again to 200 °C at a heating rate of 10 °C/min. For nonisothermal crystallization process, once the sample was annealed at 200 °C, the sample was cooled down to room temperature at different cooling rates (5, 10, 20 and 40 °C/min). Subsequently, the sample was heated again to 200 °C. All the measurements were carried out in nitrogen atmosphere.

A Wide angle X-ray diffraction (WAXD, Panalytical X'pert PRO diffractometer with Ni-filtered Cu K $\alpha$  radiation) was used to characterize the crystal structure of PP-MA and nucleated PP-MA obtained after being isothermal crystallized at 135 °C. The continuous scanning angle range was from 5° to 35° at 40 kV and 40 mA. The  $\beta$ -phase fraction ( $K_\beta$ ) in the sample was calculated from WAXD diffractograms according to the following relation [16]:

$$K_\beta = I_{300}^\beta / (I_{110}^\alpha + I_{040}^\alpha + I_{130}^\alpha + I_{300}^\beta) \quad (1)$$

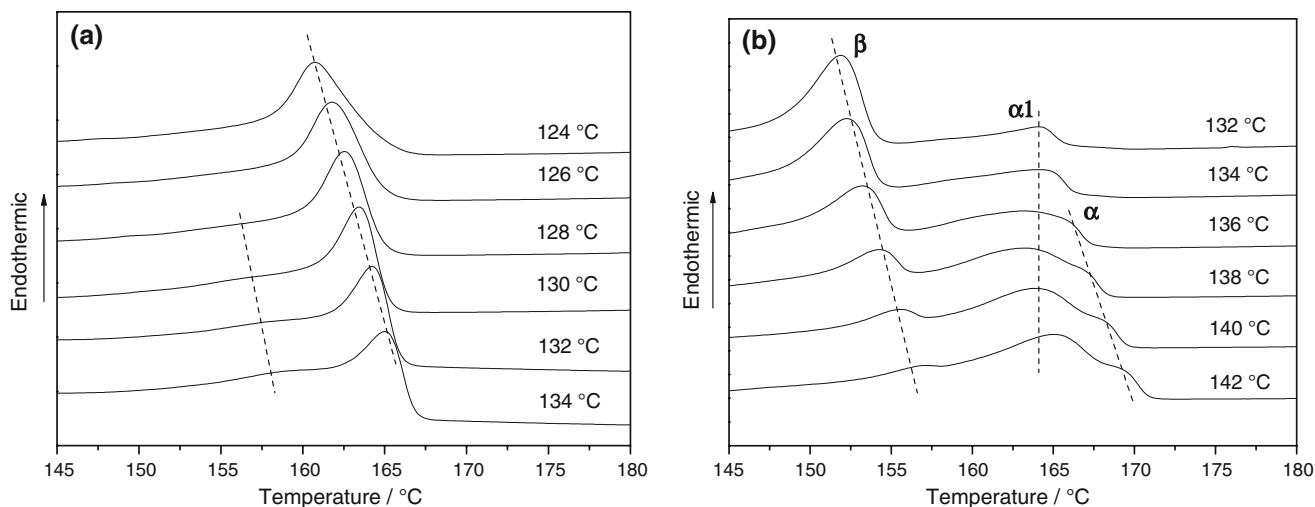
where  $I_{110}^\alpha$ ,  $I_{040}^\alpha$  and  $I_{130}^\alpha$  are the integral intensities of the (110), (040) and (130) reflections of  $\alpha$ -phase, respectively, appearing at  $2\theta$  around 14.1, 16.9, 18.4°, respectively, and  $I_{300}^\beta$  is the integral intensity of (300) reflection of  $\beta$ -phase at  $2\theta$  around 16.1°.

The crystallization morphology of sample obtained through isothermal crystallization at 135 °C was characterized by a polarized light microscopy (XPN-203, China).

## Results and discussion

### Isothermal crystallization and subsequent melting behaviors

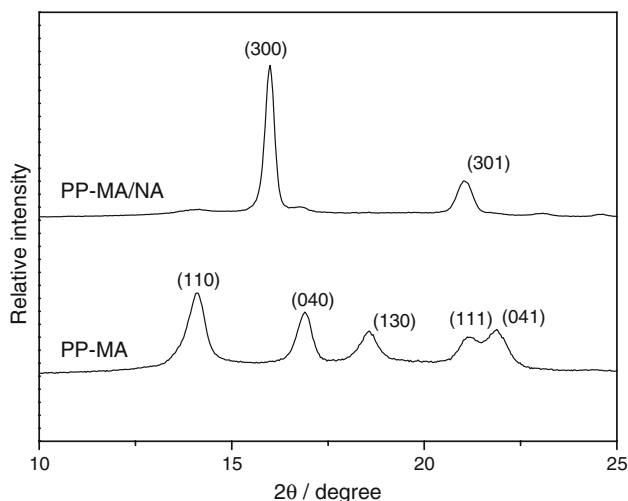
Figure 1 shows the DSC heating curves of neat PP-MA and PP-MA/NA after isothermal crystallization at different temperatures as indicated. It can be observed that the peak temperature shifts to high temperatures with the increase of crystallization temperature ( $T_c$ ), indicating thicker lamellae formation at relative higher  $T_c$ . For neat PP-MA, one can see that when  $T_c$  is below 130 °C, only a single melting peak is observed, otherwise, double melting peaks with a weak shoulder peak location at lower temperature are observed, indicating the formation of some lamellae with defect or smaller thickness at higher  $T_c$ , possibly due to the second crystallization in the interface of spherulites. PP-MA/NA sample presents double melting peaks at about 152.5–157 °C and 165 °C at low  $T_c$ . The left melting peak is ascribed to the fusion of  $\beta$ -phase, and the right one to  $\alpha$ -phase (Shown as  $\beta$  and  $\alpha_1$ , respectively) [17]. It also can be seen that the relative amount of  $\beta$ -phase gradually decreases with the increase of  $T_c$  applied in the work, and when crystallization temperature is at 142 °C,  $\beta$ -phase content is very small. This is due to the temperature is



**Fig. 1** DSC heating curves of **a** PP-MA and **b** PP-MA/NA samples after isothermal crystallization at the indicated temperatures

higher than the appropriate temperature for the  $\beta$ -phase growth (100–140 °C) [18]. When  $T_c$  is higher than 136 °C, a weak melting peak ( $\alpha_2$ ) at about 167–169 °C appears besides  $\alpha_1$ , this shoulder peak gets stronger and shifts to high temperatures with the increase of  $T_c$ , possibly due to the fusion of reorganized  $\alpha$ -phase from the melting of  $\beta$ -phase and poor perfect  $\alpha$ -phase during the heating process [19].

To further prove the nucleation effect of TMB-5 on crystallization of PP-MA, isothermal crystallized neat PP-MA and PP-MA/NA samples were comparatively investigated through using WAXD and PLM, respectively, and the results are shown in Figs. 2 and 3. From Fig. 2 one can see that neat PP-MA crystallizes mainly in  $\alpha$ -phase and PP-MA/NA mainly in  $\beta$ -phase. The relative content of  $\beta$ -phase was calculated as 75% according to the method



**Fig. 2** WAXD profiles of PP-MA and PP-MA/NA. Samples were obtained after isothermal crystallization at 135 °C

proposed by Turner-Jones A [16], indicating that TMB-5 is very efficient as a  $\beta$ -phase NA in inducing PP-MA crystallization. This also can be proved by the crystallization morphology obtained during the isothermal crystallization. As shown in Fig. 3, neat PP-MA exhibits spherulites with diameters of about 100–200  $\mu\text{m}$ , whereas much more homogeneous spherulites with diameters of about 5–10  $\mu\text{m}$  are observed for PP-MA/NA sample, which means that the presence of TMB-5 increases the nucleation density of PP-MA greatly during the crystallization process.

Figure 4 shows the heat flow evolutions of virgin PP-MA and PP-MA/NA versus crystallization time. Although the  $T_c$  is different for virgin PP-MA and PP-MA/NA, one can notice that, once NA is introduced into PP-MA, the crystallization rate is enhanced greatly, shorter induction period of crystallization and narrower crystallization peaks are obtained in PP-MA/NA sample compared with neat PP-MA.

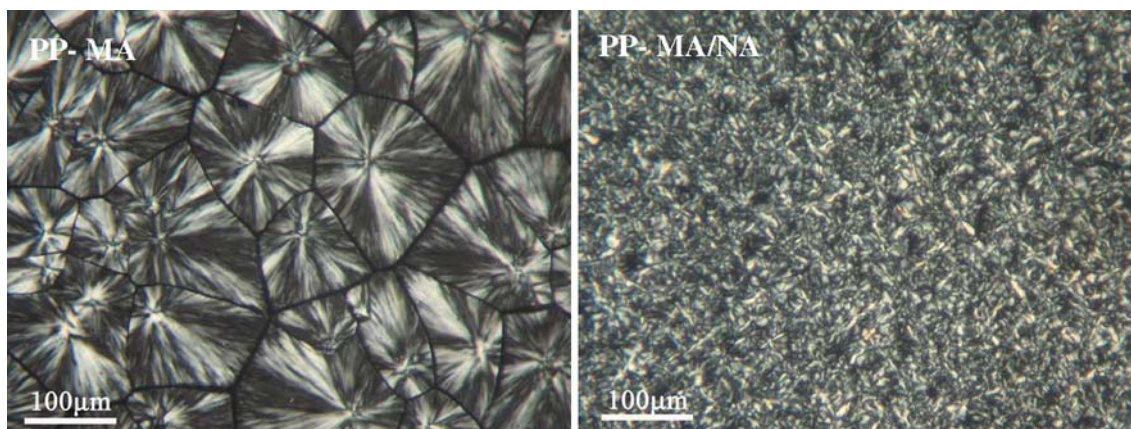
The isothermal crystallization of polymers can usually be well described by the Avrami equation [20]:

$$1 - X_t = \exp(-Kt^n) \quad (2)$$

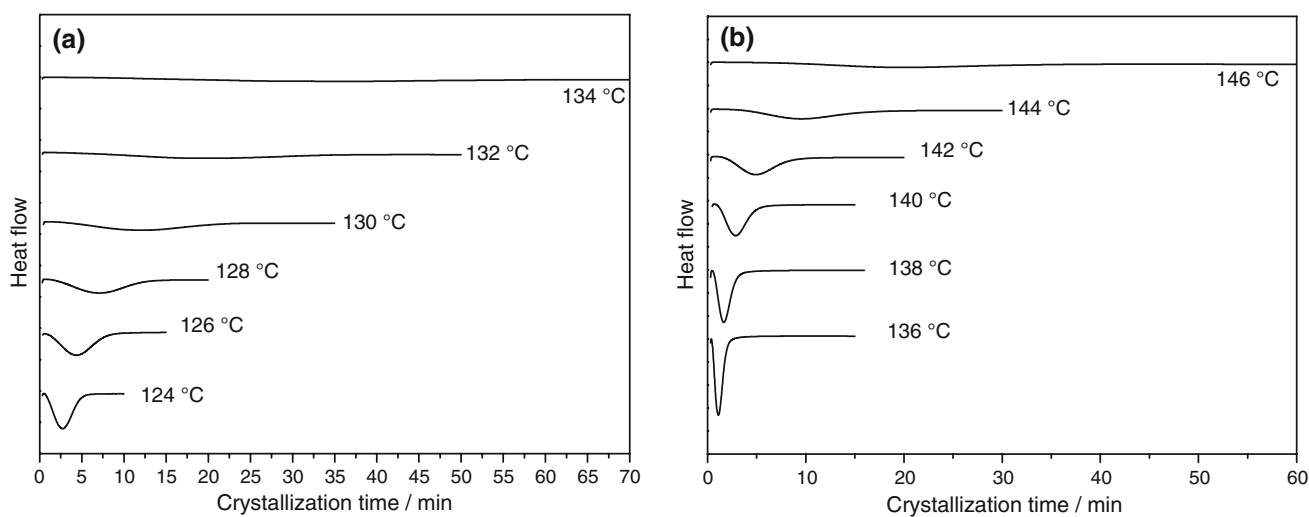
where  $X_t$  is the relative degree of crystallinity at time  $t$ ,  $n$  is the “Avrami exponent” which depends on the type of nucleation and the growth mechanism during the crystallization,  $K$  is a rate constant related to nucleation and growth rate parameters, and  $t$  is the time elapsed from the start of phase transformation. According to the Avrami equation, one formula can be got as follows:

$$\lg[-\ln(1 - X_t)] = n \lg t + \lg K \quad (3)$$

And generally, the plot of  $\lg[-\ln(1 - X_t)]$  versus  $\lg t$  is a straight line. The slope of the line is  $n$  and the intercept with the ordinate yields  $\lg K$ . From Eq. 3 the crystallization half time  $t_{1/2}$  can be obtained by



**Fig. 3** PLM images of isothermal crystallization morphologies of PP-MA and PP-MA/NA



**Fig. 4** DSC heat flow curves of **a** PP-MA and **b** PP-MA/NA samples during the isothermal crystallization process

$$t_{1/2} = (\ln 2/k)^{1/n} \quad (4)$$

Figure 5 shows the plots of  $\lg [-\ln(1 - X_t)]$  versus  $\lg t$ , and the corresponding isothermal crystallization kinetics parameters are shown in Table 1. It is evident that, whether for neat PP-MA or for PP-MA/NA, the plots exhibit straight lines in the whole crystallization, which indicates that Avrami equation can satisfactorily describe the isothermal crystallization of PP-MA and PP-MA/NA and suggests that the crystallization of such samples is an one-step process. As shown in Table 1, PP-MA/NA sample has much smaller  $t_{1/2}$  than PP-MA, suggesting the faster crystallization process. Furthermore, both PP-MA and PP-MA/NA exhibit the Avrami exponent values  $n$  of about 2–3, indicating that spherulite development arises from an athermal heterogeneous nucleation [21]. For neat PP-MA, it can be ascribed to a heterogeneous nucleation followed by diffusion-controlled spherulite growth due to

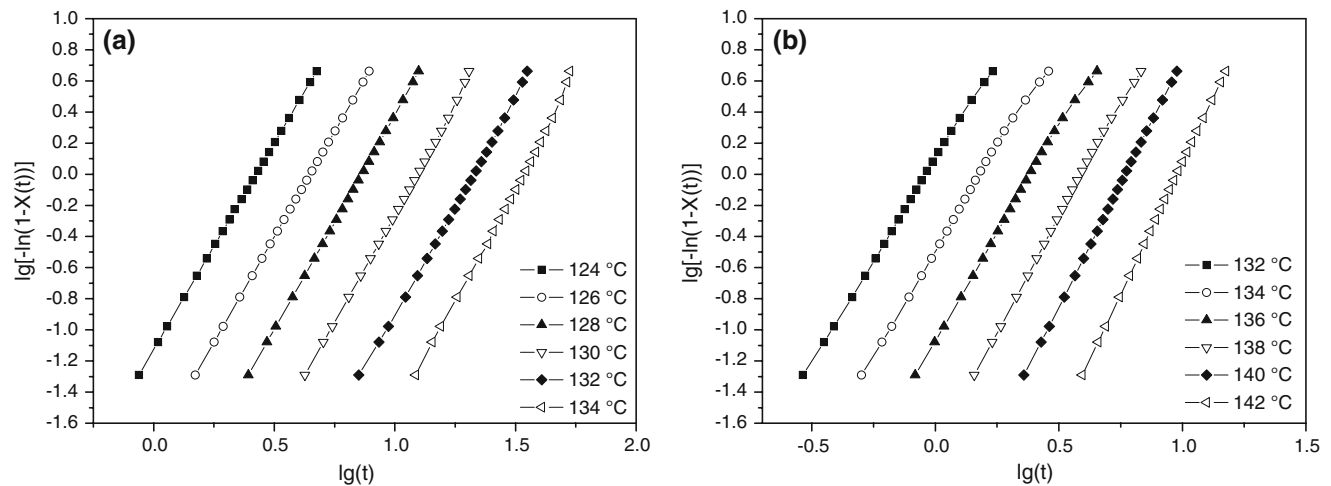
the existence of impurities and catalyst residues during the chemical modification of PP.

The kinetic data of polymer isothermal crystallization can be analyzed using the spherulitic growth rate of the Hoffman-Lauritzen secondary nucleation theory, especially at melt-crystallization condition [22, 23].

$$G = G_0 \exp\left[\frac{-U^*}{R(T_c - T_\infty)}\right] \exp\left[\frac{-K_g}{T_c \cdot \Delta T \cdot f}\right] \quad (5)$$

$$\ln G + \frac{U^*}{R(T_c - T_\infty)} = \ln G_0 - \frac{K_g}{T_c \cdot \Delta T \cdot f} \quad (6)$$

where  $G_0$  is a constant of pre-exponential factor independent of temperature;  $U^*$  is the parameters describing the activation energy characteristic of the transport of the crystallizing segments across the liquid–crystal interface, universally  $U^* = 6,280$  J/mol;  $R$  is the gas constant;  $T_\infty$  is the theoretical temperature at which all motions associated



**Fig. 5** Avrami plots of  $\lg[-\ln(1 - X_t)]$  vs.  $\lg t$  for **a** PP-MA and **b** PP-MA/NA

**Table 1** Isothermal crystallization kinetic parameters of neat PP-MA and PP-MA/NA

	PP-MA						PP-MA/NA					
$T_c$ (°C)	124	126	128	130	132	134	132	134	136	138	140	142
$n$	2.66	2.71	2.74	2.76	2.78	2.85	2.53	2.63	2.71	2.94	3.08	3.33
$\bar{n}$	2.75						2.87					
$\lg k$	-1.33	-1.76	-2.37	-3.02	-3.69	-4.38	0.06	-0.51	-1.07	-1.75	-2.40	-3.28
$t_{1/2}$ (min)	2.31	3.89	6.39	10.90	18.65	30.14	0.82	1.36	2.17	3.49	5.32	8.60
$T_m^M$ (°C)	160.7	161.9	162.5	163.5	164.3	165.0	152.3	153.2	154.3	155.5	157.2	158.6
$T_m^O$ (°C)	188.6						173.4					
$\sigma_e$ (mJ/m <sup>2</sup> )	98.14						35.61					
$\sigma$ (mJ/m <sup>2</sup> )	11.49						10.48					
$K_g$ (10 <sup>5</sup> K <sup>2</sup> )	4.81						1.50					
$L_m$ (nm)	16.54	17.27	17.70	18.40	19.03	19.57	8.52	8.89	9.42	10.05	11.09	15.15

with the viscous flow ceases and is defined as  $T_\infty = T_g - C$ , here  $C$  is a constant and in this paper  $C \approx 30$  K;  $\Delta T$  denotes the undercooling ( $\Delta T = T_m^0 - T_c$ ), here  $T_m^0$  is an equilibrium melting temperature;  $f$  is a corrective factor responsible for the variation of the equilibrium melting enthalpy with temperature, defined as  $f = 2T_c/(T_m^0 + T_c)$ ; and  $K_g$  is a nucleation constant as defined as:

$$K_g = 4b_0\sigma\sigma_e T_m^0 / \Delta h_f k \quad (7)$$

where  $b_0$  is the monolayer thickness,  $\sigma$  is the lateral surface free energy,  $\sigma_e$  is the fold surface free energy,  $k$  is the Boltzmann constant ( $k = 1.38 \times 10^{-23}$  J/K), and  $\Delta h_f$  is the enthalpy of fusion.

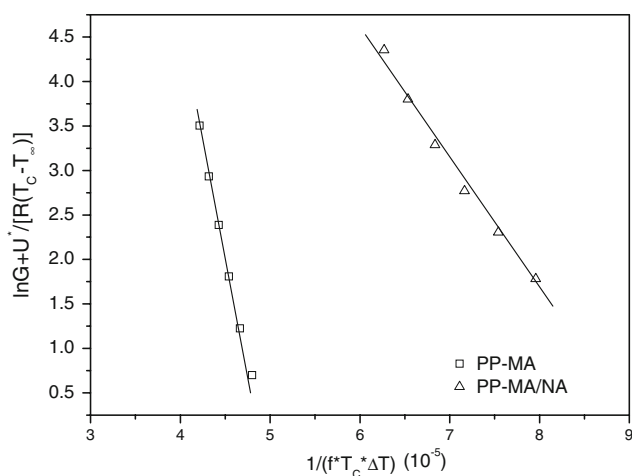
Equations 5–7 are applied for crystallization occurring in regimes I and III. From Eq. 6, the slope of plot of  $\ln G + U^*/R(T_c - T_\infty)$  versus  $1/T_c \cdot \Delta T \cdot f$  is  $K_g$ . From Eq. 7,  $K_g$  can be used to calculate the fold surface free energy  $\sigma_e$ . The plots of  $\ln G + U^*/R(T_c - T_\infty)$  versus  $1/T_c \cdot \Delta T \cdot f$  for neat PP-MA and PP-MA/NA and corresponding  $K_g$  values are shown in Fig. 6 and Table 1,

respectively. Prior to determining  $\sigma_e$ ,  $\sigma$  is estimated through using the following equation:

$$\sigma = \alpha(a_0 b_0)^{1/2} \Delta h_f \quad (8)$$

where  $\alpha$  is assumed empirically to be 0.1; and  $a_0 b_0$  is the cross-sectional area of the chain. For  $\alpha$ -phase PP, the crystal growth is estimated in favor along (110) lattice plane during melt-crystallization; for  $\beta$ -phase PP, the crystal growth is estimated in favor along (300) lattice plane. Thus, the value of  $a_0 b_0$  is  $3.44 \times 10^{-19}$  and  $3.50 \times 10^{-19}$  m<sup>2</sup> for  $\alpha$ -PP and  $\beta$ -PP, respectively. And  $\Delta h_f$  is  $1.96 \times 10^8$  J/m<sup>3</sup> for  $\alpha$ -PP and  $1.77 \times 10^8$  J/m<sup>3</sup> for  $\beta$ -PP [24, 25].

The fold surface free energy  $\sigma_e$  of virgin PP-MA and PP-MA/NA are shown in Table 1 too. As expected, the addition of NA results in smaller  $K_g$  and  $\sigma_e$  values. Generally, surface nucleation barrier is positive proportion to  $K_g$  [23] and the increase of  $\sigma_e$  goes against the folding of the molecule chain [26]. Beck's theory thought that a good NA reduced the interfacial surface free energy [27]. The



**Fig. 6** Plot of  $\ln G + U^* / [R(T_c - T_\infty)]$  vs.  $1/T_c \cdot \Delta T \cdot f$  for PP-MA and PP-MA/NA

smaller the  $\sigma_e$  value, the better the nucleation effect of NA is. Table 1 shows that TMB-5 has good nucleation effect for PP-MA.

The lamella thickness formed during the isothermal crystallization process was calculated according to the equation developed by Thomson and Gibbs [28]:

$$T_m = T_m^0 [1 - 2\sigma_e / (l\Delta h_f)] \quad (9)$$

where  $l$  is the lamellar thickness,  $T_m$ ,  $\sigma_e$ , and  $\Delta h_f$  are defined as previous. According to Thomson-Gibbs equation, the lamellar thickness of a polymer can be calculated as follows:

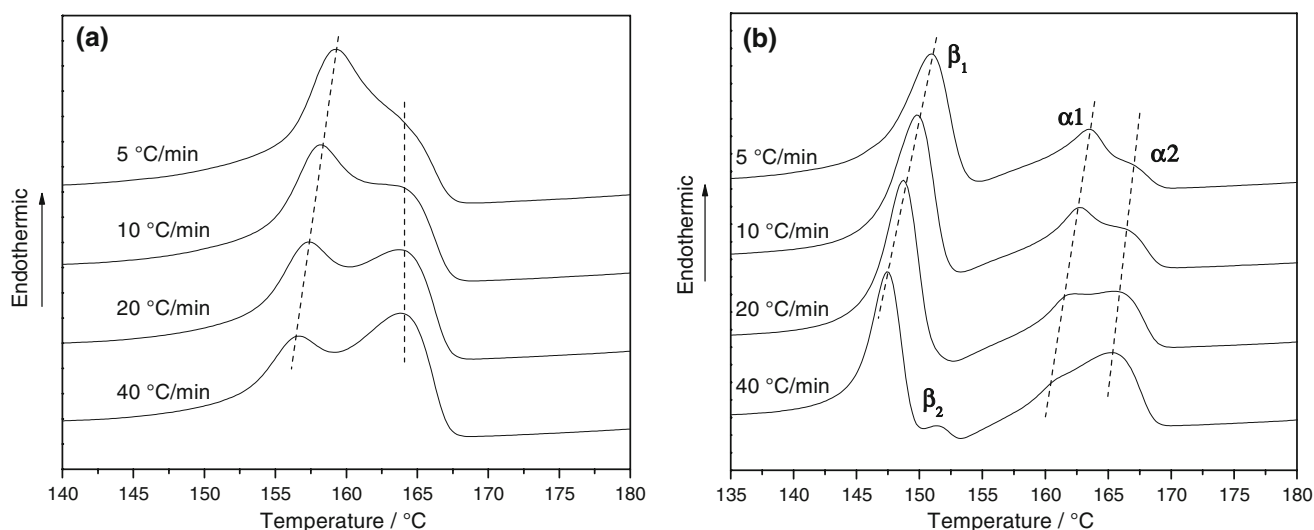
$$l = 2\sigma_e T_m^0 / [\Delta h_f (T_m^0 - T_m)] \quad (10)$$

Prior to calculating the lamellar thickness, one must know the value of equilibrium melting temperature, which

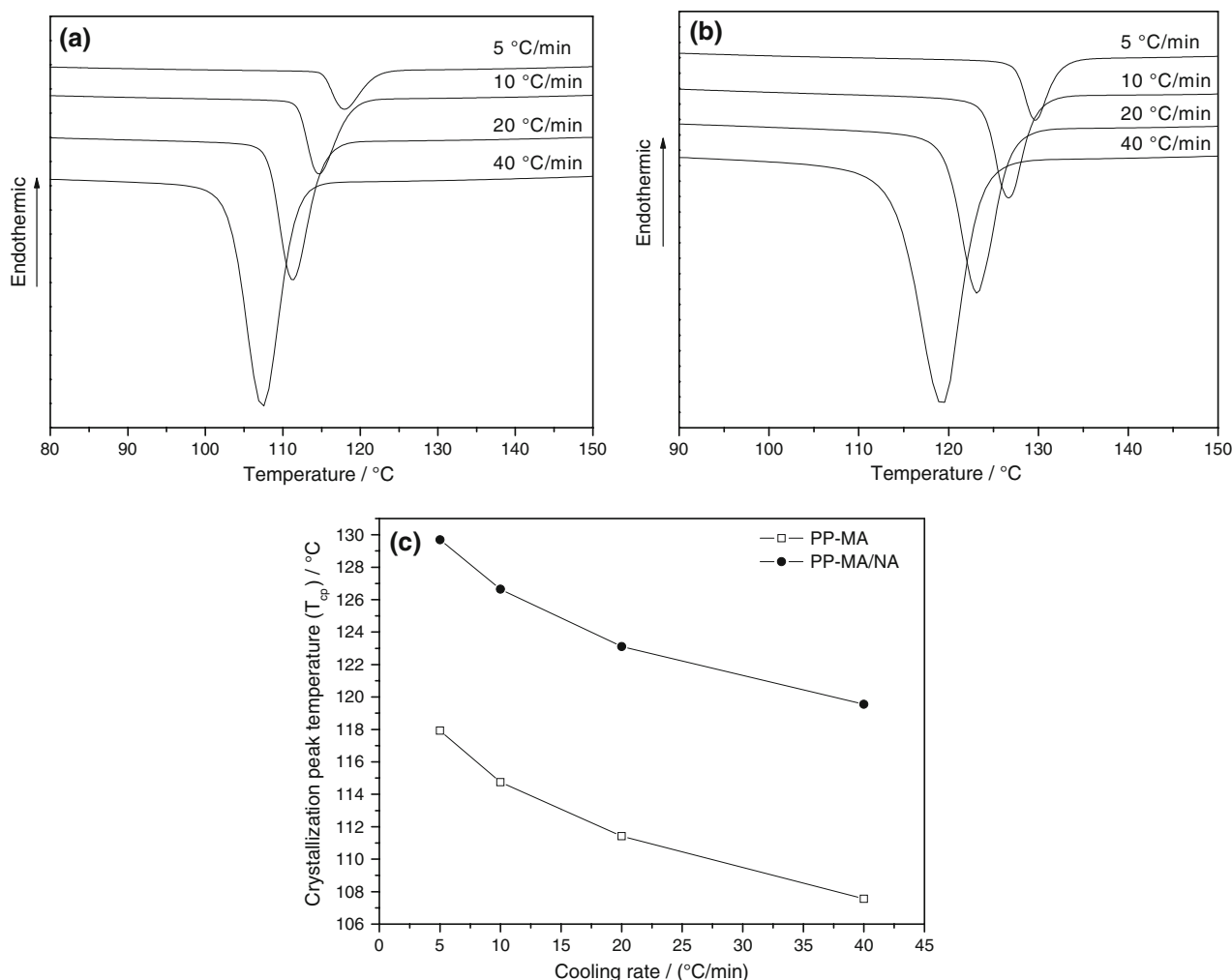
can be obtained by linear extrapolating the experimental data to  $T_m = T_c$  line based on Hoffman-Weeks theory [26]. Here, the  $T_m^0$  for neat PP-MA and PP-MA/NA are calculated as 188.6 and 173.4 °C. As shown in Table 1, the lamella thickness increases with increasing of  $T_c$ , indicating more perfect spherulites formation at higher temperature. Furthermore, the addition of NA results in the decrease of lamella thickness, although the nucleated sample crystallizes at relative higher temperature. Considering the main crystal forms in virgin PP-MA ( $\alpha$ -phase) and in PP-MA/NA ( $\beta$ -phase), it can be proved that, for PP-MA,  $\alpha$ -phase shows bigger lamella thickness than that of  $\beta$ -phase.

### Nonisothermal crystallization and subsequent melting behaviors

Study on the nonisothermal crystallization behavior is very important because polymer usually faces the temperature gradients and the crystallization is normally the nonisothermal crystallization during the processing. In this section, the nonisothermal crystallization and subsequent melting behaviors of neat PP-MA and PP-MA/NA were comparatively researched. Figure 7 shows the DSC heating curves of such samples after nonisothermal crystallization at different cooling rates as indicated. Interestingly, neat PP-MA presents double melting peaks, one is present at about 156–159 °C ( $\alpha_1$ ) and the other ( $\alpha_2$ ) at 164 °C.  $\alpha_1$  shifts to lower temperatures and gets weaker intensity with the increasing of cooling rate, whereas  $\alpha_2$  keeps invariant temperature but gets stronger intensity. Obviously, the grafted maleic anhydride prevents the nucleation and lamella growth of PP-MA, resulting in the formation of



**Fig. 7** DSC heating curves of **a** PP-MA and **b** PP-MA/NA after nonisothermal crystallization at different cooling rates. The data show the corresponding cooling rates



**Fig. 8** DSC cooling curves of **a** PP-MA and **b** PP-MA/NA samples during the nonisothermal melt crystallization at different cooling rates. **c** shows the crystallization peak temperature versus cooling rate

spherulites with more defects compared with isotactic PP. Thus, it can be deduced that  $\alpha_1$  is related to the fusion of the lamella with defects and  $\alpha_2$  is attributed to the fusion of lamella formed due to recrystallization or reorganization of lamella initially formed during nonisothermal crystallization [29]. Three melting peaks, 147–151 °C ( $\beta$ ), 161–163.5 °C ( $\alpha_1$ ) and 165–167 °C ( $\alpha_2$ ), are observed for all the nonisothermal crystallized PP-MA/NA samples. These melting peaks shift to lower temperatures with the increasing of cooling rate, indicating the formation of more imperfect lamella structure. Compared with the melting behavior of isothermal crystallized sample, one can see that nonisothermal crystallized sample exhibits relative lower melting temperature, indicating the formation of lamella with more defects or smaller thickness.

The typical DSC cooling traces obtained at different cooling rates are shown in Fig. 8. Especially, the corresponding crystallization peak temperatures ( $T_{cp}$ ) at different cooling rates were determined from the cooling curves and

the results are shown in Fig. 8 too. For all the samples, the  $T_{cp}$  decreases with increasing cooling rate. This is attributed to the dependence of nucleation and crystal growth on the degree of supercooling. A small cooling rate provides better fluidity and diffusivity for molecules due to low viscosity and more time for crystallization, thus inducing higher crystallinity at higher temperature, than for a sample cooled with a fast cooling rate [30]. Neat PP-MA has smaller  $T_{cp}$  due to the relative homogeneous nucleation process and the relative low nucleation density. For PP-MA/NA, the  $T_{cp}$  is much higher than that of neat PP-MA, further indicating the great nucleation effect of TMB-5 for PP-MA crystallization.

## Conclusions

In summary, an aryl amide derivative (TMB-5) has been introduced into PP-MA and the crystallization and subsequent melting behaviors of TMB-5 nucleated PP-MA

have been intensively researched based on isothermal and nonisothermal crystallization process, respectively. The results show that TMB-5 is an efficient  $\beta$ -NA in inducing PP-MA crystallization as  $\beta$ -phase with largely increased crystallization rate, decreased fold surface free energy and decreased lamella thickness.

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